

TECHNICAL MEMORANDUM

DATE May 27, 2014 **PROJECT No.** 13-1118-0010 (5008)

TO Alexandra Drapack
Osisko Hammond Reef Gold Ltd.

DOC No. 0033 (Rev 1)

FROM Devin Hannan, P.Eng. EMAIL dhannan@golder.com

OSISKO HAMMOND REEF GOLD PROJECT – TAILINGS MANAGEMENT FACILITY, 3D GROUNDWATER MODELLING

1.0 INTRODUCTION

The purpose of this technical memorandum is to report on three-dimensional (3D) groundwater modelling of the eastern portion of the proposed Tailings Management Facility (TMF) for the Hammond Reef Gold Project and the adjacent Lizard Lake catchment area (Figure 1). The objectives of the modelling analysis are as follows:

- Simulate groundwater flow within and around the eastern portion of the TMF; and
- Evaluate applicability of the design concept for seepage collection.

The seepage collection system design is currently at a conceptual level and includes perimeter ditches and collection ponds. As such, a rigorous modelling analysis is not required at this time. Instead, the model described herein is used to evaluate the applicability of the conceptual design in terms of seepage collection such that it may be considered a practical basis for future designs. This modelling will be updated in the future for the purposes of detailed engineering design and regulatory permitting as new hydrogeological data is collected following approval of the Hammond Reef Gold Project Environmental Impact Statement/Environmental Assessment (Osisko, 2013).

2.0 TAILINGS MANAGEMENT FACILITY DESIGN

The modelled TMF layout is based on the design framework put forth in the technical memorandum *Design Basis for Runoff and Seepage Collection Systems – Hammond Reef Gold Project* (Golder, 2013¹) included in the *Hydrogeology Technical Support Document (Version 2)* (Golder, 2013²). The TMF is proposed to store 165 Mm³ of thickened tailings over a footprint of approximately 800 ha throughout five stages of tailings deposition and progressive dam raise construction. The modelling focusses on the TMF at the ultimate extent, as this configuration would produce the greatest amount of groundwater flow.

The conceptual design for the TMF containment system includes rockfill dams with upstream geomembrane liners. The reclaim pond dams will be fully lined, whereas the upstream rockfill dam shells will be lined on the lower (approximate) half of their upstream flank. Runoff and water released from the tailings due to consolidation/settlement will be collected in the TMF reclaim pond (located south of the TMF). Groundwater seepage will be collected by perimeter collection ditches and conveyed to collection ponds where it will be pumped back to the TMF reclaim pond.



3.0 HYDROGEOLOGICAL DATA

The primary source of hydrogeological data for model construction is *Hydrogeology Technical Support Document (Version 2)* (Golder, 2013²). This TSD includes site borehole logs, hydraulic testing, and grain size analysis summaries. The following information from the TSD is pertinent to the model construction:

- The average overburden depth within the model domain is 5 m;
- Bedrock weathering is not typically observed in borehole logs within the model domain; however, where present, the weathered thickness is less than 3 m;
- The geometric mean hydraulic conductivity of the coarse grained material in the TMF area is 6E-6 m/s; and
- The geometric mean hydraulic conductivity of the upper bedrock zone in the TMF area is 2E-6 m/s.

Figure 1 shows the location of site boreholes and their respective overburden depths. The borehole logs within the model domain (and BRH-0019, which lies slightly outside of the model domain but is included in this analysis) are provided in Appendix A of this memorandum.

4.0 MODEL CONSTRUCTION

A summary of model input parameters and boundary conditions are provided in Table 1. Additional information is as follows:

- Code: MODFLOW-2005 (Harbaugh, 2005) is the code used to simulate groundwater flow at the site. MODFLOW is a multi-purpose three dimensional groundwater flow code developed by the United States Geological Survey. It is modular in nature and uses the finite difference formulation of the groundwater flow equation in its solution. MODFLOW has been recognized as an industry standard for general purpose groundwater flow modelling and has gained wide acceptance from academia, consultants and regulatory agencies worldwide. Visual MODFLOW® (Version 2011.1) is used as the pre and post-processor for the simulations presented in this report. SAMG (Algebraic Multigrid Methods for Systems) is used to solve the groundwater flow equations.
- **Domain:** The groundwater model domain is shown on Figure 1. The domain is limited to the eastern TMF as this is the area where seepage would be directed towards Lizard Lake; the remaining western TMF area would discharge towards Sawbill Bay. As such, the western flank of the model is ascribed according to the future topographic divide created by the tailings mound. The eastern boundary of the model is represented by Lizard Lake. The remaining model outline is delineated according to subcatchment divides.
- Layout: The MODFLOW representation of the TMF and surrounds is displayed on Figure 2 (model layer 1 shown).
- Layers: The nominal model layering is as follows: 1) Tailings and lake bathymetry (Lizard Lake depth taken from Golder, 2013³); 2) Dam Materials (Upper); 3) Dam Materials (Lower); 4) Overburden; 5) Weathered Bedrock; 6) Competent Bedrock. Note that it is necessary to subdivide the dam geometry as the tailings dams only have liner on the approximate lower half of their upstream shell, whereas the reclaim pond dam has liner along its entire upstream shell. For a given layer, where the nominal material is not present, the numerical layer thins out to 1 m and the underlying material property is input in its stead.
- Hydraulic Conductivity: A "bulk" approach to assigning hydraulic conductivities to each unit is utilized. Spatial differentiation of hydraulic conductivities within units is not considered warranted given the scope of



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this model analysis. Isotropic conditions are assumed at each material with the exception of the overburden, which is assigned a $K_H:K_Z$ of 1:0.1. This anisotropy is selected due to the presence of clayey lenses within the overburden material that would tend to impede vertical flow.

- Geomembrane Liner: The geomembrane liner is considered impermeable (inactive cells) in the model. However, there is the potential that future "wear and tear" of the liner may increase the effective permeability the material. This could result in some shallow seepage crossing the rockfill dams; however, this seepage would ultimately report to the perimeter seepage collection ditches and be captured.
- Perimeter Seepage Collection Ditches: The seepage collection ditches are represented by drain cells at a depth of 7 m below existing ground surface.
- **Cross-Section**: A west-east cross-section through the model domain is shown on Figure 3.

5.0 MODEL RESULTS

Figure 4 displays the simulated water table surface. Groundwater flows from a high at the tailings radially outward, eventually discharging to either the perimeter seepage collection ditching, drainage features upstream of Lizard Lake or to Lizard Lake itself.

Table 2 lists the model flow budget. The term "in" means into the *groundwater* system, whereas "out" means out of the *groundwater* system. The total amount of water entering and leaving the modelled groundwater system is 1,954 m³/d.

Inflows: Most of the inflow to the model is provided by the tailings (712 m^3/d) and reclaim pond (1,240 m^3/d). Some flow occurs within the tailings themselves, a result of constant head cells at higher elevations "feeding" adjacent cells at lower elevations – this is a normal and expected numerical outcome given the representation of the tailings water table surface as sloped constant heads. It follows that the net groundwater flow emanating from the TMF is 712 m^3/d – 395 m^3/d = 317 m^3/d . Note that a small portion of inflow, 2 m^3/d , occurs from the Lizard Lake upstream drainage to Lizard Lake itself. This is a result of the drainage feature having a higher head elevation than the downstream Lizard Lake.

Outflows: For this given conceptual design the majority of the outflow reports to the perimeter collection ditches (1,409 m³/d). The remainder of outflow reports to the Lizard Lake catchment (146 m³/d total).

Seepage Collection: Also provided in Table 2 is a breakdown of flows as they pertain to collection ditch efficiency for the conceptual design. A total of 1,409 m³/d of the 1,553 m³/d of groundwater emanating from the TMF is retained. These results reflect a capture efficiency of 91%. This is consistent with the treatment efficiency used in the EIS/EA (Osisko, 2013).

6.0 CONCLUSIONS

A 3D MODFLOW groundwater model is constructed to simulate flow in and around the eastern portion of the TMF and Lizard Lake and to estimate the capture efficiency of the proposed seepage collection system conceptual design. The modelling analysis suggests that a capture efficiency of greater than 90% is achievable using a perimeter seepage collection ditch of 7 m or greater. It follows that the seepage collection system conceptualization forms a reasonable basis for future detailed design, and that values used in the EIS/EA evaluation is reasonable and appropriate.



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7.0 RECOMMENDATIONS

It is recommended that, as the conceptual design is advanced during pre- construction stages, the model should in turn be refined to provide more exacting estimates of seepage and continue to assist in the design finalization. With a more refined model, a sensitivity analysis may be performed to determine an upper and lower bound on results.

8.0 REFERENCES

Golder, 2013¹. Design Basis for Runoff and Seepage Collection Systems – Hammond Reef Gold Project. Document No. 011 (Rev 0). Project No. 13-1118-0010 (2010). Submitted to Osisko Hammond Reef Gold Ltd. December 3, 2013.

Golder, 2013². *Hammond Reef Gold Project, Hydrogeology Technical Support Document, Version 2.* Document No. DOC017. Project No. 13-1118-0010. Submitted to Osisko Hammond Reef Gold Ltd. December 2013.

Golder, 2013³. *Hammond Reef Gold Project, Aquatic Environment Technical Support Document, Version 2.* Document No. DOC013. Project No. 13-1118-0010. Submitted to Osisko Hammond Reef Gold Ltd. December 2013.

Harbaugh, A.W., 2005. MODFLOW-2005, The U.S. Geological Survey Modular Ground-Water Model - the Ground-Water Flow Process. U.S. Geologic Survey Techniques and Methods 6-A16.

Osisko (Osisko Hammond Reef Gold Ltd.), 2013. *Hammond Reef Gold Project, Environmental Impact Statement/Environmental Assessment Report. Version 2.* Submitted to Canadian Environmental Assessment Agency and Ontario Ministry of the Environment. December 2013. Toronto, ON.

9.0 CLOSURE

We trust this meets your current requirements. If you have any questions please do not hesitate to contact the undersigned.

<Original signed by>

<Original signed by>

Devin Hannan, P.Eng. Associate, Environmental Engineer Ken De Vos, M.Sc., P.Geo. Principal

DAH/KD/sp

Attachments:

Table 1 – Summary of Model Construction Details

Table 2 - Model Flow Budget

Figure 1 – General Arrangement Plan Tailings Management Facility

Figure 2 – Model Layout (Layer 1)

Figure 3 – Model Cross-section

Figure 4 – Simulated Water Table (masl)

Appendix A – Borehole logs

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TABLES

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TABLE 1 Summary of Model Construction Details

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| General Attributes | | | |
|------------------------|---------------------------------|--|--|
| Code | USGS MODFLOW 2000 | | |
| Software | Visual MODFLOW Version 2011.1 | | |
| Flow Type | Steady-State | | |
| Dimensions | 3D | | |
| | | | |
| Domain | | | |
| Area | 10 km ² | | |
| Horizontal Extents | 2 km wide x 5 km long | | |
| Vertical Extents | 492 masl to 400 masl | | |
| Top of Model | Ground Surface (see Figure 1) | | |
| Bottom of Model | 400 masl (competent rock layer) | | |
| | | | |
| Grid Layout | | | |
| Grid Spacing | 10 m x 10 m to 20 m x 20 m | | |
| Number of Layers | 6 | | |
| Number of Active Cells | 538,314 | | |

| Numerical Layer D | | | |
|-------------------|--------------------------------|-------------|--------------------|
| Layer | Nominal Description | Thickness | Notes |
| 1 | Tailings and Lake Bathymetry | 62 m to 1 m | |
| 2 | Rockfill Dam and Liner (Upper) | 14 m to 1 m | Liner ~ 1 m thick. |
| 3 | Rockfill Dam and Liner (Lower) | 14 m to 1 m | Liner ~ 1 m thick. |
| 4 | Overburden | 5 m - 7 m | |
| 5 | Weathered Bedrock | 3 m | |
| 6 | Competent Bedrock | 80 m to 1 m | |

| Material Properties | | | |
|---------------------|---|--------------------------------|---------------------------|
| Material | Hydraulic Conductivity K _H (m/s) | K _H :K _Z | Source |
| Tailings | 6E-07 | 1:1 | (Golder, 2012) |
| Water Bodies | 1E-02 | 1:1 | Assumed |
| Rockfill | 1E-04 | 1:1 | Assumed |
| Geomembrane Liner | Impermeable | 1:1 | Assumed |
| Overburden | 6E-06 | 1:0.1 | Golder, 2013 ² |
| Weathered Bedrock | 2E-06 | 1:1 | Golder, 2013 ² |
| Competent Bedrock | 2E-08 | 1:1 | Assumed |

| Boundary Conditions | | | | | |
|---------------------------|-------------------------------|------------------|---------------------------|--|--|
| Feature | Туре | Assigned Head | Source | | |
| Tailings Phreatic Surface | Constant Head | Ground minus 2 m | Assumed | | |
| Reclaim Pond | Constant Head | 444.5 masl | Golder, 2013 ² | | |
| Seepage Collection Ditch | Drains (Conductance 500 m²/d) | Ground minus 7 m | Iterative modelling. | | |
| Lizard Lake U/S Drainage | Constant Head | 430 masl | Golder, 2013 ² | | |
| Lizard Lake | Constant Head | 426.65 masl | Golder, 2013 ³ | | |
| External Catchment Areas | Inactive | - | Golder, 2013 ² | | |

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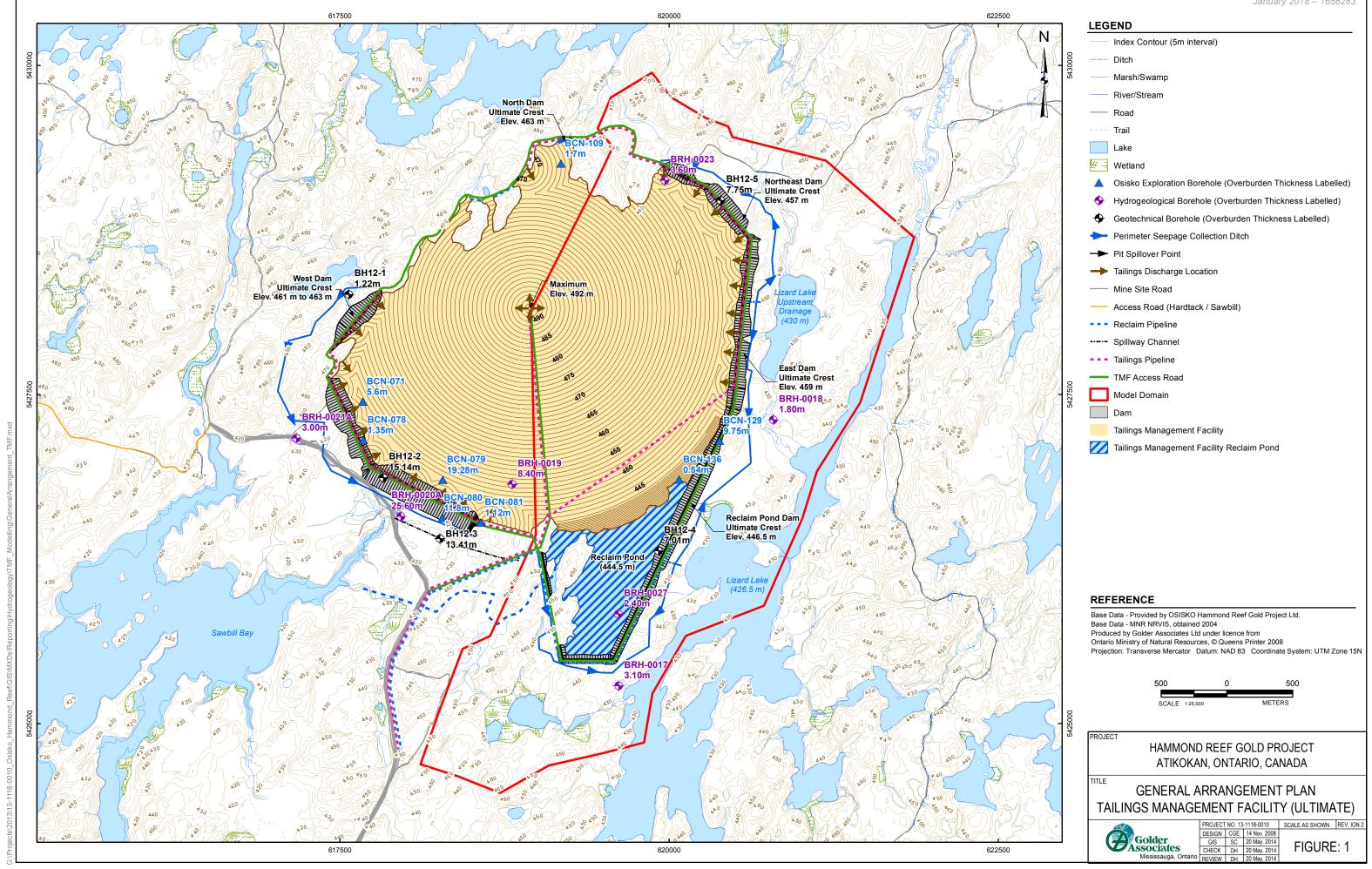
TABLE 2 Model Flow Budget

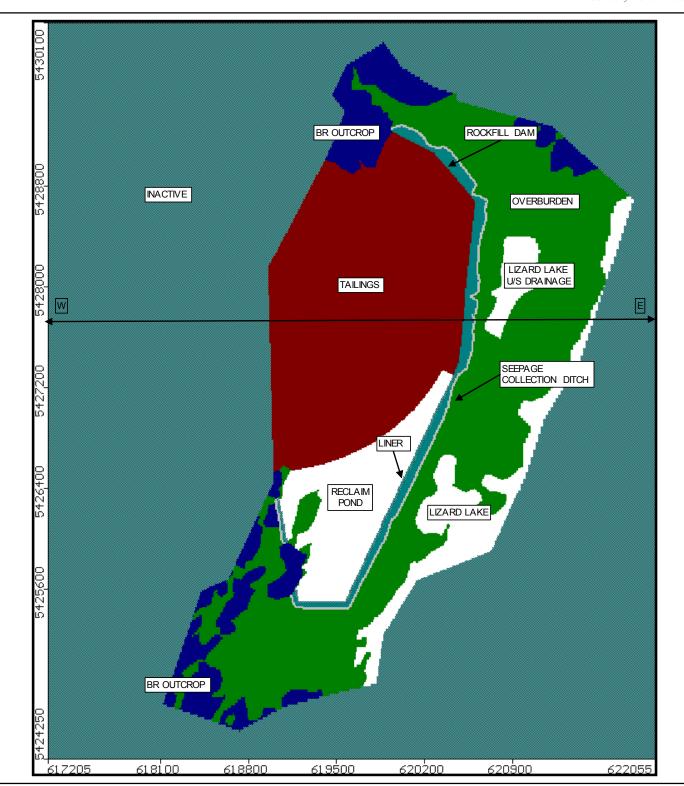
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| Global Flow Balance | | | | | |
|---------------------------------|---------------|-----------------------------|------------------------------|----------------------|--|
| Feature | Boundary Type | Flow In (m ³ /d) | Flow Out (m ³ /d) | Net In (+) / Out (-) | |
| Tailings | CH | 712 | 395 | 317 | |
| Reclaim Pond | CH | 1,240 | 4 | 1,236 | |
| Northeast Dam Collection Trench | Drains | 0 | 110 | -110 | |
| East Dam Collection Trench | Drains | 0 | 196 | -196 | |
| Reclaim Pond Collection Trench | Drains | 0 | 1,103 | -1,103 | |
| Lizard Lake | CH | 0 | 126 | -126 | |
| Lizard Lake Upstream Drainage | CH | 2 | 20 | -18 | |
| | TOTAL: | 1,954 | 1,954 | 0 | |

| TMF Groundwater Flow Details | | | | |
|--|-------|--|--|--|
| Total Groundwater Flow External To TMF (m ³ /d) | 1,553 | | | |
| Tailings Seepage Collected (m³/d) | 306 | | | |
| Reclaim Pond Seepage Collected (m ³ /d) | 1,103 | | | |
| Bypass to Lizard Lake and Lizard Lake Drainage (m³/d) | 144 | | | |
| Collection Efficiency (%) | 91 | | | |
| Bypass to Lizard Lake Catchment (%) | 9 | | | |

FIGURES





LEGEND

| UNIT | DESCRIPTION |
|------|--------------------|
| | WATER BODY |
| | TAILINGS |
| | ROCKFILL DAM |
| | OVERBURDEN |
| | WEATHERED BEDROCK |
| | COLLECTION DITCH |
| | INACTIVE / NO FLOW |

| PROJECT | HAMMOND REEF GOLD PROJECT |
|---------|---------------------------|
| | ATIKOKAN, ONTARIO, CANADA |

TITLE

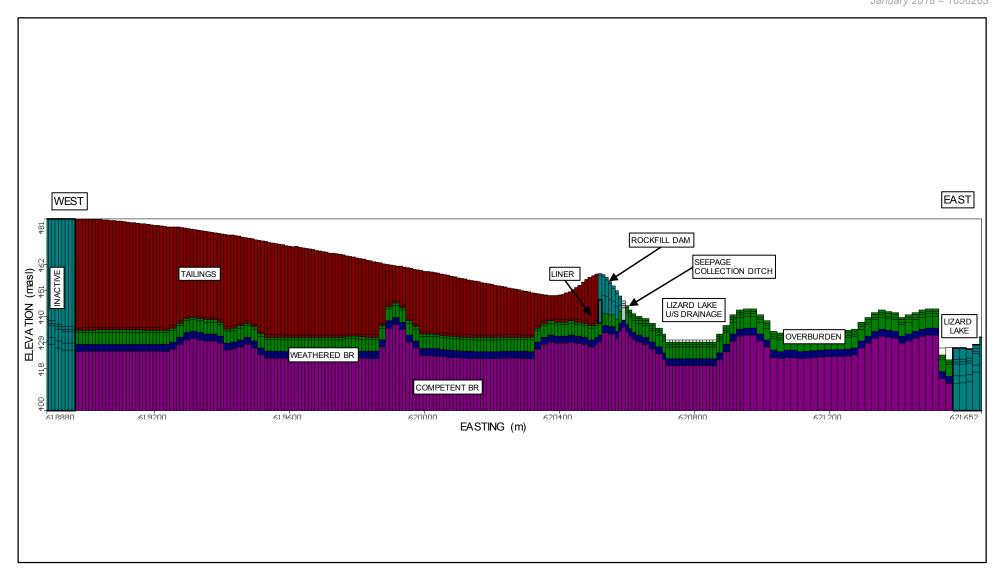
MODEL LAYOUT (LAYER 1)

| Golder |
|---------------------|
| Associates |
| Mississaura Ontario |

| | PROJECT | | | |
|---|---------|----|--------------|-----|
| | DESIGN | SC | 5 May. 2014 | |
| | GIS | SC | 21 May. 2014 | |
| | CHECK | DH | 21 May. 2014 | FIG |
|) | REVIEW | DH | 21 May. 2014 | |

REV. 0.0





LEGEND

| ı | UNIT | DESCRIPTION |
|---|------|--------------------|
| ı | | WATER BODY |
| | | TAILINGS |
| I | | ROCKFILL DAM |
| I | | OVERBURDEN |
| I | | WEATHERED BEDROCK |
| I | | COLLECTION DITCH |
| ı | | INACTIVE / NO FLOW |

HAMMOND REEF GOLD PROJECT
ATIKOKAN, ONTARIO, CANADA

TITLE

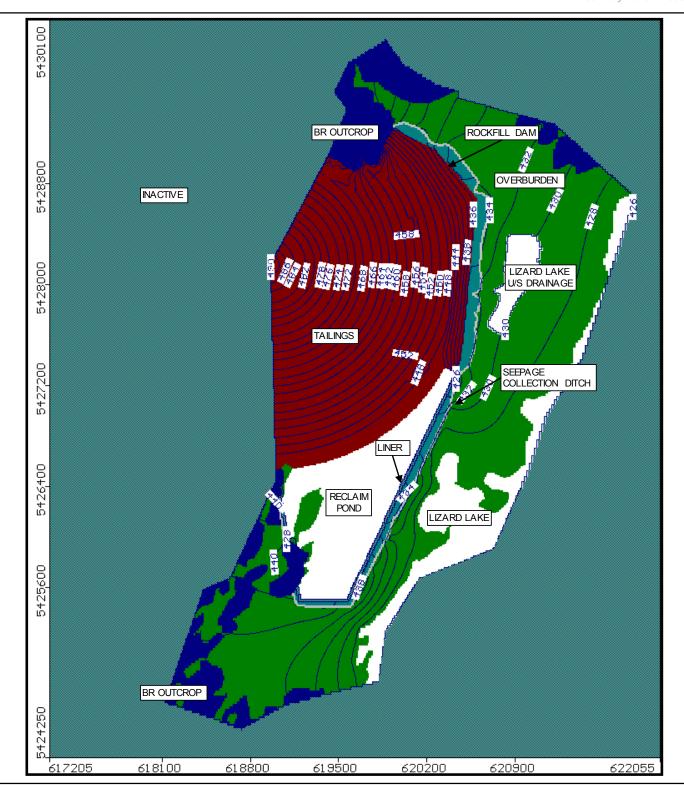
MODEL CROSS-SECTION

| | PRU |
|----------------------|-----|
| | DES |
| Golder | 0 |
| Associates | СН |
| Mississauga, Ontario | RF\ |

| PROJECT | NO. 13 | -1118-0010 | |
|---------|--------|--------------|--|
| DESIGN | SC | 5 May. 2014 | |
| GIS | SC | 21 May. 2014 | |
| CHECK | DH | 21 May. 2014 | |
| REVIEW | DG | 21 May. 2014 | |

FIGURE: 3

REV. 0.0



LEGEND

| UNIT | DESCRIPTION |
|------|--------------------|
| | WATER BODY |
| | TAILINGS |
| | ROCKFILL DAM |
| | OVERBURDEN |
| | WEATHERED BEDROCK |
| | COLLECTION DITCH |
| | INACTIVE / NO FLOW |

PROJECT HAMMOND REEF GOLD PROJECT ATIKOKAN, ONTARIO, CANADA

TITLE

SIMULATED WATER TABLE (masl)

| As As | Golder Sociates |
|-------|---------------------|
| | Mississauga, Ontari |

PROJECT NO. 13-1118-0010

DESIGN SC 5 May. 2014

GIS SC 21 May. 2014

CHECK DH 21 May. 2014

PROJECT NO. 13-1118-0010

DESIGN SC 21 May. 2014

REV. 0.0

APPENDIX A 6 cfY\ c`Y``c[g

SHEET 1 OF 1

RECORD OF BOREHOLE: BRH-0017A

LOCATION: N 5425289.5 ;E 619623.7 BORING DATE: April 7, 2011 DATUM: Geodetic

PROJECT: 10-1118-0020 / 4000

SAMPLER HAMMER, 63.5 kg; DROP, 760 mm PENETRATION TEST HAMMER, 63.5 kg; DROP, 760 mm INCLINATION: -90 degrees

| ا پر | 2 | | SOIL PROFILE | 1. | | SA | MPLE | | AMIC PEI ISTANCE | NETRA' , BLOW | 110N /S/0.3m | (| HYDRAUL k, | IC COND cm/s | UC FIVITY | ΄, Τ | RG A B | PIEZOMETER |
|-----------------------|--------------|----------------------------------|--|-------------|-----------------------|--------|--------------|--------------------|---------------------|------------------|-------------------|--------------------------|---|-----------------|--|---------------------------------|----------------------------|-----------------------------------|
| DEPTH SCALE METRES | COLTEM SINIO | BORING ME | DESCRIPTION | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | SHE Cu, F | AR STRE | 40 NGTH 40 | nat V rem V. 6 | 80 + Q - ● → U - ○ | 10 ⁻⁶ WATE Wp ⊢ 16 | | 10 ⁻⁴ ENT PER W 48 | 10 ⁻³ CENT -I WI 64 | ADDITIONAL LAB. TESTING | OR STANDPIPE INSTALLATION |
| - 0 | | | GROUND SURFACE Loose, moist to wet, brown, silty SAND, some organics. | | 424.6 0.0 | 1 | 50 DO | | 20 | 40 | | 00 | 16 | 32 | 40 | 64 | | Cement |
| 1 | 2 | w Stem Auger) | | | | 2 | 50 DO 5 | 5 | | | | | | | | | | Bentonite Holeplug Riser |
| 2 | CME 55 | 200 mm Diam. (Hollow Stem Auger) | Loose to compact, wet, brown, SAND, some silt, some clay, trace gravel. | | 423.1 1.5 | 3 | 50 DO 2 |) | | | | | | | | | МН | Silica Sand |
| 3 | | | Compact, wet, brown, medium to coarse, SAND, trace to some gravel, trace silt. | | 422.3 2.3 | 4 | B0 | 3 | | | | | | | | | | |
| 4 | | | Fresh bedding, grey, very coarse-grained, crystalline, strong rock (TONALITE). | | 3.1 | 5 | 50 5 DO 0 | " 1- | | | | | | | | | | Bentonite Holeplug |
| 5 | CME 55 | NQ Core | | | | | | | | | | | | | | | | Silica Sand |
| 7 | | | END OF DODE NO. 5 | | 417.4 | | | | | | | | | | | | | 31.8 mm Diam. PVC #10 Slot Screen |
| 8 | | | END OF BOREHOLE Note: 1. For coring details see Record of Drillhole BRH-0017A. | | 7.2 | | | | | | | | | | | | | U.84 m Riser Stickup. |
| 9 | | | | | | | | | | | | | | | | | | |
| 10 DE | PTI | ΉS | CALE | | | | | | | اماء | er iates | | | | | | L | OGGED: TDM |

CHECKED: MO

RECORD OF DRILLHOLE: **BRH-0017A** PROJECT: 10-1118-0020 / 4000 SHEET 1 OF 1 DRILLING DATE: April 7, 2011 DATUM: Geodetic LOCATION: N 5425289.5 ;E 619623.7 DRILL RIG: CME 55 Trackmount INCLINATION: -90° AZIMUTH: ---DRILLING CONTRACTOR: George Downing Estate Drilling Ltd. PL - Planar CU- Curved UN- Undulating ST - Stepped IR - Irregular PO- Polished
K - Slickensided
SM- Smooth
RO- Rough
MB- Mechanical Break

BR - Broken Rock
NOTE: For additional abbreviations refer to list of abbreviations & symbols. JN - Joint FLT - Fault SHR- Shear VN - Vein CJ - Conjugate BD- Bedding FO- Foliation CO- Contact OR- Orthogonal CL - Cleavage DRILLING RECORD DEPTH SCALE METRES SYMBOLIC LOG ELEV. DESCRIPTION HYDRAULIC CONDUCTIVITY k, cm/s DEPTH RECOVERY DISCONTINUITY DATA R.Q.D. FRACT. INDEX METRES Diametra Joint Loa Index (MPa) DIP w.r.t. CORE AXIS (m) TOTAL SOLID CORE % 0000 8848 2320 TOP OF BEDROCK 421.50 Fresh, bedding, grey, very coarse-grained, crystalline, strong rock (TONALITE). Silica Sand **JPLR** Bentonite Holeplug JPLR JPLSM 5 CME 55 NQ Core JIR JIR Silica Sand JPLR JPLR JPLR JPLR JPLR JPLR JIR - JIR 31.8 mm Diam. PVC #10 Slot 3 417.4 0.84 m Riser Stickup. END OF DRILLHOLE 8 10 11 12 13 DEPTH SCALE LOGGED: TDM

10-1118-0020 (4000).GPJ GAL-MISS.GDT 21/09/12 DATA INPUT

1:50

SHEET 1 OF 1

RECORD OF BOREHOLE: BRH-0017B

LOCATION: N 5425289.5 ;E 619623.7 BORING DATE: April 7, 2011 DATUM: Geodetic

SAMPLER HAMMER, 63.5 kg; DROP, 760 mm PENETRATION TEST HAMMER, 63.5 kg; DROP, 760 mm INCLINATION: -90 degrees

| SHEAR STRENGTH nat V. + Q ● WATER CONTENT PERCENT Wp - W W 16 32 48 64 | PIEZOMETER | | ₽g₽ | Ţ | | | | HYDRAU k | \ | ON /0.3m | ETRATION BLOWS | IIC PEN TANCE, | DYNA! RESIS | PLES | SAM | | T. 1 | SOIL PROFILE | | 요 | |
|--|---------------------------------|--------------|--------------------------|----|-------|-------|--------|-------------|---|-------------|----------------|-------------------|----------------|-----------|--------|----------------|------------|---|------------------|---------------------|--------|
| CROCAND SURFACE | OR STANDPIPE INSTALLATION | | ADDITION/ LAB. TESTIN | IT | PERCE | NTENT | TER CO | WAT | | 1 | | | | LOWS/0.3m | NUMBER | ELEV. DEPTH | TRATA PLOT | DESCRIPTION | DE | ORING MET | METRES |
| Refer to Borehold BRH-0017A for strating upphy defails. Day | | \vdash | | ļ. | 3 6 | 2 4 | 32 | 16 |) | 3 08 | 0 6 | 0 4 | 2 | - B | - | , | S | IRFACE | GROLIND SLIDE | \rightarrow | + |
| 2.3 Screen 3.1 4.2.6 3.1 END OF BOREHOLE Note: 1. Monitoring well installation in same Borehole as BRH-0017A. | 29/10/11 | Ben | | | | | | | | | | | | | | 0.0 | | ehole BRH-0017A for | Refer to Borehol | | 1 |
| END OF BOREHOLE Note: 1. Monitoring well installation in same Borehole as BRH-0017A. | nm Diam. #10 Slot | 31.8 PV0 | | | | | | | | | | | | | | 1.5 425.4 | | | | 200 mm Diam. (Hollo | |
| END OF BOREHOLE Note: 1. Monitoring well installation in same Borehole as BRH-0017A. 8 | | | | | | | | | | | | | | | | | | | | | |
| 420.5 END OF BOREHOLE Note: 1. Monitoring well installation in same Borehole as BRH-0017A. | | | | | | | | | | | | | | | | | | | | NQ Core | |
| 1. Monitoring well installation in same Borehole as BRH-0017A. | n Riser up. | 0.8° Stic | | | | | | | | | | | | | | | | REHOLE | | | 7 |
| | | | | | | | | | | | | | | | | | | g well installation in same BRH-0017A. | | - 1 | 8 |
| | | | | | | | | | | | | | | | | | | | | | 9 |
| | | | | | | | | | | | | <u>.</u> | 200 | | | | | | | | 10 |

PROJECT: 10-1118-0020 / 4000

RECORD OF BOREHOLE: BRH-0018

PROJECT: 10-1118-0020 / 4000

1:50

SHEET 1 OF 1

CHECKED: MO

LOCATION: N 5427310.9 ;E 620793.8 BORING DATE: March 28, 2011 DATUM: Geodetic SAMPLER HAMMER, 63.5 kg; DROP, 760 mm PENETRATION TEST HAMMER, 63.5 kg; DROP, 760 mm

INCLINATION: -90 degrees DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m HYDRAULIC CONDUCTIVITY, k, cm/s SOIL PROFILE SAMPLES DEPTH SCALE METRES BORING METHOD ADDITIONAL LAB. TESTING PIEZOMETER STRATA PLOT BLOWS/0.3m NUMBER STANDPIPE INSTALLATION ELEV. TYPE SHEAR STRENGTH nat V. + Q - ● rem V. ⊕ U - ○ WATER CONTENT PERCENT DESCRIPTION DEPTH -OW Wp ⊢ (m) GROUND SURFACE 430.6 Loose, moist, brown, CLAYEY SAND and SILT 50 DO РН 0 МН CME 55 50 DO 2 15 Compact, moist, brown to grey, silty SAND, trace to some gravel. 50 50/ DO 0.28 3 0 428.8 27/10/11 Fresh, grey, very coarse-grained, crystalline, strong rock (quartz GRANITE) Bentonite Holeplug Riser CME 55 NQ Core 31.8 mm Diam. PVC #10 Slot Screen Silica Sand SUD-BOREHOLE 10-1118-0020 (4000).GPJ GLDR_CAN.GDT 21/09/12 DATA INPUT: 421.9 0.97 m Riser END OF BOREHOLE 1. For coring details see Record of Drillhole BRH-0018. 10 DEPTH SCALE LOGGED: TDM

CHECKED: MO

RECORD OF DRILLHOLE: BRH-0018 PROJECT: 10-1118-0020 / 4000 SHEET 1 OF 1 DRILLING DATE: March 28, 2011 DATUM: Geodetic LOCATION: N 5427310.9 ;E 620793.8 DRILL RIG: CME 55 Trackmount INCLINATION: -90° AZIMUTH: ---DRILLING CONTRACTOR: George Downing Estate Drilling Ltd. PL - Planar CU- Curved UN- Undulating ST - Stepped IR - Irregular PO- Polished
K - Slickensided
SM- Smooth
RO- Rough
MB- Mechanical Break

BR - Broken Rock
NOTE: For additional abbreviations refer to list of abbreviations & symbols. JN - Joint FLT - Fault SHR- Shear VN - Vein CJ - Conjugate BD- Bedding FO- Foliation CO- Contact OR- Orthogonal CL - Cleavage DRILLING RECORD DEPTH SCALE METRES SYMBOLIC LOG ELEV. DESCRIPTION RUN HYDRAULIC CONDUCTIVITY k, cm/s DEPTH RECOVERY DISCONTINUITY DATA R.Q.D. FRACT. INDEX METRES Diametra Joint Loa Index (MPa) DIP w.r.t. CORE AXIS (m) TOTAL SOLID CORE % 0000 8848 2320 TOP OF BEDROCK 428.80 Fresh, grey, very coarse-grained, 1.80 crystalline, strong rock (quartz GRANITE) Bentonite Holeplug JIR Closely Fractured Closely Fractured 3 JIR Healed Joint JPLR JIR Riser JIR JIR CME 55 NQ Core 31.8 mm Diam. PVC #10 Slot Screen Silica Sand JSTR 5 JIR JIR 421.9 8.7 END OF BOREHOLE 0.97 m Riser Stickup. 10 11 Golder DEPTH SCALE LOGGED: TDM

10-1118-0020 (4000).GPJ GAL-MISS.GDT 21/09/12 DATA INPUT

1:50

RECORD OF BOREHOLE: BRH-0019

PROJECT: 10-1118-0020 / 4000 LOCATION: N 5426821.6 ;E 618808.1 BORING DATE: March 19, 2011 SHEET 1 OF 1 DATUM: Geodetic

SAMPLER HAMMER, 63.5 kg; DROP, 760 mm PENETRATION TEST HAMMER, 63.5 kg; DROP, 760 mm INCLINATION: -90 degrees

| , F | 9 | } | SOIL PROFILE | | 1 | SA | MPL | | DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m | HYDRAULIC CONDUCTIVITY, k, cm/s | AL NG | PIEZOMETER |
|-----------------------|---------------|----------------------------------|--|-------------|-----------------------|--------|----------|------------|--|---|----------------------------|--|
| DEPTH SCALE METRES | BORING METHOD | | DESCRIPTION | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | BLOWS/0.3m | 20 40 60 80 SHEAR STRENGTH nat V. + Q - ● Cu, kPa rem V. ⊕ U - ○ | 10 ⁶ 10 ⁵ 10 ⁴ 10 ³ WATER CONTENT PERCENT Wp W W | ADDITIONAL LAB. TESTING | OR STANDPIPE INSTALLATION 26/10/11 |
| | | + | GROUND SURFACE | N. | 430.6 | | | Е | 20 40 60 80 | 16 32 48 64 | | 26/10/11 |
| 0 | П | 1 | Wet, dark brown, PEAT (ORGANICS). | EEE | 0.0 | | | | | | | Silica Sand |
| | | - 1 | Wet, dark brown, sandy SILT and ORGANICS (TOPSOIL). | | 430.3 0.3 430.0 | | 50 DO | 3 | | 0 | | Bentonite Holeplug |
| | | | Grey-brown to brown, layered, SILTY, CLAYEY SAND, oxidized mottling. | | 0.6 | | | | | | | Riser |
| 1 | | | | | | 2 | 50 DO | 5 | | 0 | МН | |
| 2 | | | Wet, brown, layered, clayey SILT, some sand, oxidized mottling. | | 429.1 1.5 | 3 | 50 DO | 25 | | | | Riser |
| 1 | | | | | | 4 | 50 DO | 28 | | H O I | МН | Cuttings |
| 3 | | | Moist to wet, grey, layered, SILTY CLAY, | | 427.6 3.0 | | БО | | | | | |
| | | | trace sand to CLÁY, some silt, trace sand | | | 5 | 50 DO | 26 | | | | Riser |
| 4 | CME 55 | 200 mm Diam. (Hollow Stem Auger) | | | | 6 | 50 DO | 22 | | 0 | | Bentonite Holeplug |
| 5 | | 200 mm D | | | | 7 | 50 DO | 27 | | | МН | [3, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, |
| | | | | | | 8 | 50 DO | 15 | | 0 | МН | |
| 6 | | | | | | 9 | 50 DO | 15 | | | | Silica Sand 31.8 mm Diam. PVC #10 Slot Screen |
| 7 | | | | | | 10 | 50 DO | 11 | | 0 | | |
| 8 | | | Wet, brown, medium to coarse, granitic, SAND, trace silt. | | 423.0 7.6 | | 50 DO | 2 | | | | |
| | Ш | _ | END OF BOREHOLE | X | 422.2 | | | | | | | Cave 83 m Riser |
| 9 | | | PROBABLE BEDROCK REFUSAL | | | | | | | | | Stickup. |
| 10 | | | | | | | | | | | | |
| DE 1: | | -1 S0 | CALE | <u> </u> | 1 | 1 | | | Golder Associates | | | L OGGED: MO IECKED: MO |

SHEET 1 OF 1

RECORD OF BOREHOLE: BRH-0023

LOCATION: N 5429127.4 ;E 619973.0 BORING DATE: March 26, 2011 DATUM: Geodetic

SAMPLER HAMMER, 63.5 kg; DROP, 760 mm PENETRATION TEST HAMMER, 63.5 kg; DROP, 760 mm INCLINATION: -90 degrees

| . FE | 5 | | SOIL PROFILE | 1 - | | SA | MPLE | | AMIC PE STANCE | | | , | k | LIC COND , cm/s | | | RG ING | PIEZOMETER |
|----------|--------------|----------------------------------|--|-------------|------------------------------|--------|----------|---|---------------------|-------------|-------------|--------------------------|---------------------------------|------------------------------|----|---------------------------|----------------------------|--|
| METRES | COLTAM SINIO | OKING ME | DESCRIPTION | STRATA PLOT | ELEV. DEPTH (m) | NUMBER | TYPE | | 20 AR STRE Pa | 40 ENGTH | 1 | 80 + Q - ● • U - ○ | 10 ⁻⁶ WAT Wp F | 10 ⁻⁵ TER CONT | | 10 ⁻³ CENT WI | ADDITIONAL LAB. TESTING | OR STANDPIPE INSTALLATION |
| \dashv | _ | <u>"</u> | GROUND SURFACE | S | | | | ٥ | 20 | 40 | 60 | 80 | 16 | 32 | 48 | 64 | | |
| 0 | | П | Boulders and TOPSOIL. | ĒĒĒ | 434.9 | | | | | | | | | | | | | |
| | | - | Moist to wet, greyish-brown, SILT and SAND, trace organics. | | 434.4 0.5 | | | | | | | | | | | | | 27/10/11 Bentonite Holeplug |
| 1 | | Auger) | Wet, brown, gravelly SILT and SAND. | | 433.6 1.3 433.4 | 1 | 50 DO | 1 | | | | | 0 | | | | МН | Riser |
| | | v Sterr | Wet, brown, SAND and GRAVEL, some clay, trace silt, trace cobbles and | MIT | 433.4 | | | - | | | | | | | | | | Ŗ |
| 2 | CME 55 | 200 mm Diam. (Hollow Stem Auger) | clay, trace silt, trace cobbles and boulders. | | | 2 | 50 DO | 1 | | | | | 0 | | | | МН | |
| | | 200 mn | SAND and BOULDERS, some gravel, trace silt. Gravelly SAND, some silt, trace clay. | | 432.6 2.3 432.2 2.7 | 3 | 50 DO | 2 | | | | | | | | | | Silica Sand 31.8 mm Diam. PVC #10 Slot Screen |
| 3 | | | | | | | | | | | | | | | | | | |
| | | | | | 431.3 | 4 | 50 DO | 3 | | | | | 0 | | | | МН | Cave In |
| | | | END OF BOREHOLE PROBABLE BEDROCK REFUSAL | | 3.6 | | | | | | | | | | | | | 0.9 m Riser Stickup. |
| 5 | | | | | | | | | | | | | | | | | | |
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| DEI | PTI | ΉS | CALE | l | 1 | | <u> </u> | Â | 7 | - Fold | er iates | 1 | 1 | | | | L | DGGED: MO |

PROJECT: 10-1118-0020 / 4000

Vanuary 2018 – 165020 SHEET 1 OF 1

RECORD OF BOREHOLE: BRH-0027

LOCATION: N 5425831.2 ;E 619613.6 BORING DATE: April 8, 2011 DATUM: Geodetic

SAMPLER HAMMER, 63.5 kg; DROP, 760 mm INCLINATION: -90 degrees PENETRATION TEST HAMMER, 63.5 kg; DROP, 760 mm

| SA | IVIP | LEF | RHAMMER, 63.5 kg; DROP, 760 mm | | | | | | INCLINATION: | -90 de | grees | | | PENE | TRATIO | N IESI | HAIVIIVII | ER, 63 | .5 kg; DROP, 760 mm |
|-----------------------|---------------|----------------------------------|---|-------------|----------------|--------|----------|-------------|----------------------------|-----------------|----------------------|-------|----------|-------------------|-------------------|-------------------|-----------|----------------------------|---|
| Э- | 2 | 3 | SOIL PROFILE | | | SA | MPL | ES | DYNAMIC PEN RESISTANCE, | ETRATI BLOWS | ON S/0.3m | 1 | HYDRA | ULIC C k, cm/s | ONDUCT | TIVITY, | T | l G | PIEZOMETER |
| DEPTH SCALE METRES | BORING METHOD | | | STRATA PLOT | | i. | | .3m | 20 4 | 0 (| 60 8 | 30 `\ | 10 |) ⁻⁶ 1 | 0 ⁻⁵ 1 | 0 ⁻⁴ 1 | Ю-3 Т | ADDITIONAL LAB. TESTING | OR |
| MET | Č. | | DESCRIPTION | TAP | ELEV. DEPTH | NUMBER | TYPE | BLOWS/0.3m | SHEAR STREN Cu, kPa | .GTH | nat V. + rem V. ⊕ | Q - • | | | ONTENT | | | DDIT B. TE | STANDPIPE INSTALLATION |
| DE | A C B | | | STRA | (m) | Įź | | BLO | | | 60 8 | | Wp 16 | | W 32 4 | | WI 64 | \ \ | |
| | | \dashv | GROUND SURFACE | 0, | 434.8 | | | | 20 4 | , | 00 8 | | 10 | 0 3 | 2 4 | | 1 | | |
| _ 0 - | | \sqcap | Loose, moist, PEAT. | EEE | 0.0 434.6 | | | | | | | | | | | | | | - |
| - | | Ī | Loose, wet, dark brown, PEAT, some sand, some silt. | | 0.2 | 1 | 50 DO | PL | | | | | | 0 | | | | | |
| - - | | (e) | | | 434.2 | | | | | | | | | | | | | | |
| _ | | n Aug | Loose to compact, wet, grey, SANDY, SILTY CLAY | | 0.6 | _ | | | | | | | | | | | | | Bentonite Holeplug |
| - - 1 | | v Ster | | | | | 50 DO | | | | | | | | | | | МН | Riser |
| - | CME 55 | 음 | | | | 2 | DO | 8 | | | | | 9 | | | | | IVIITI | |
| | ᅙ | iam. | | | | | | | | | | | | | | | | | Silion Cond |
| | | 200 mm Diam. (Hollow Stem Auger) | | | 433.1 | | | | | | | | | | | | | | Riser Silica Sand 31.8 mm Diam. PVC#10 Slot Screen |
| | | 200 | Compact, wet, grey, coarse, SILTY SAND, some gravel, some clay. | | 1.7 | 3 | 50 DO | 13 | | | | | 0 | | | | | | Screen |
| _ 2 | | | | | | | | | | | | | | | | | | | |
| | | | | | 432.4 | 4 | 50 | 50/ 0.12 | | | | | 0 | | | | | МН | - KIKI |
| | | \exists | END OF BOREHOLE PROBABLE BEDROCK REFUSAL | | 2.4 | | | 0.12 | | | | | | | | | | | 0.95 m Riser Stickup. |
| | | | SABLE BEDITOON NEI OOME | | | | | | | | | | | | | | | | |
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| DE | PTI | H S | CALE | | | | | (| A G | olda | er | | | | | | | L | OGGED: TDM |

DEPTH SCAL 1:50

SUD-BOREHOLE 10-1118-0020 (4000).GPJ GLDR_CAN.GDT 21/09/12 DATA INPUT:

PROJECT: 10-1118-0020 / 4000

LOGGED: TDM
CHECKED: MO

CHECKED:

RECORD OF BOREHOLE: BH 12-4 PROJECT: 11-1118-0074 SHEET 1 OF 1 LOCATION: SEE FIGURE 2 DATUM: Geodetic BORING DATE: August 8 and 9, 2012 HAMMER TYPE: AUTOMATIC SPT/DCPT HAMMER: MASS, 64kg; DROP, 760mm DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m HYDRAULIC CONDUCTIVITY, k, cm/s SOIL PROFILE SAMPLES BORING METHOD ADDITIONAL -AB. TESTING DEPTH SCALE METRES PIEZOMETER STRATA PLOT 80 OR BLOWS/0.3m NUMBER STANDPIPE ELEV. TYPE SHEAR STRENGTH nat V. + Q - ● rem V. ⊕ U - O WATER CONTENT PERCENT DESCRIPTION INSTALLATION DEPTH -OW Wn F - wi (m) 428.77 **GROUND SURFACE** -0.20 (PT) Fibrous PEAT; black; wet, very 50 DO 406.8 50 mm Diameter Monitoring Well 50 DO 2 401.5 50 DO 3 320.5 2 (ML) CLAYEY SILT, trace fine sand; 2.13 grey, zones of silt; Wn<PL to Wn~PL, stiff Bentonite Seal 50 DO 10 MH TRACK MOUNTED POWER AUGER (CI) SILTY CLAY, medium plasticity, trace to some fine sand, zones of brown ф мн 72 50 DO 5 clay, zones of silt; brown to grey; cohesive, Wn>PL to Wn~PL, stiff to very stiff 200 50 DO 6 0 423.39 5.18 (ML) SILT, some fine sand; grey; wet, 50 DO 422.63 (SM) SILTY SAND, trace gravel; brown to grey; wet, loose 50 DO Silica Sand Filter 8 6 0 421.56 For bedrock coring details refer to 7.01 Record of Drillhole BH 12-4 NQ CORING GTA-BHS 001 1111180074.GPJ GAL-MIS.GDT 11/16/12 GPC AUG. 2012 1. Water encountered during drilling at a depth of 0.6 m below ground surface, Aug. 8/12 END OF BOREHOLE 2. Water level at a depth of 2.7 m below ground surface upon completion of drilling, Aug. 9/12 11 2. Water level measured in monitoring well at a height of 0.02 m (Elev. 428.59 m) above ground surface, Aug. 28/12 12 DEPTH SCALE LOGGED: AM Golder

1:63.5

CHECKED:

RECORD OF BOREHOLE: BH 12-5 PROJECT: 11-1118-0074 SHEET 1 OF 1 LOCATION: SEE FIGURE 2 DATUM: Geodetic BORING DATE: August 21, 2012 HAMMER TYPE: AUTOMATIC SPT/DCPT HAMMER: MASS, 64kg; DROP, 760mm DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m HYDRAULIC CONDUCTIVITY, k, cm/s SOIL PROFILE SAMPLES BORING METHOD ADDITIONAL LAB. TESTING DEPTH SCALE METRES PIEZOMETER STRATA PLOT 80 OR BLOWS/0.3m NUMBER STANDPIPE ELEV. TYPE SHEAR STRENGTH nat V. + Q - ● rem V. ⊕ U - O WATER CONTENT PERCENT DESCRIPTION INSTALLATION DEPTH OW Wn F (m) GROUND SURFACE В 433.03 (SM) SAND, some fines, trace to some 0.00 0 gravel; brown (FILL); moist to wet, very loose 432.73 50 DO WH 1B (PT) Fiberos (PEAT); black; wet, very 50 DO WH 2 389.8 (SP) SAND, medium grained, trace fines; brown and grey; wet, very loose 50 DO WH 1.65 3 (SM) SILTY SAND; grey; wet, loose 50 DO O. МН TRACK MOUNTED POWER AUGER 50 DO 5 9 МН 428.99 mm Dia. I (SP) SAND, some fines; grey; wet, very 200 0 6A 50 6B DO 0 (ML) SILT, some sand; grey; wet, very loose 4.88 427.47 (SW) SAND, trace gravel, some fines; 50 DO 23 0 МН (SM) gravelly SILTY SAND; grey; wet, 50 DO 50/ .13 МН For bedrock coring details refer to Record of Drillhole BH 12-5 7:7 NQ CORING 10 END OF BOREHOLE 1. Water encountered during drilling at a depth of 0.1 m below ground surface, Aug. 21/12 2. Water level at a depth of 0.3 m below ground surface upon completion of drilling, Aug. 21/12 12 DEPTH SCALE LOGGED: AM Golder

GTA-BHS 001 1111180074.GPJ GAL-MIS.GDT 11/16/12 GPC AUG. 2012

1:62